

## VARIABLE WATTAGE CONTROL SYSTEM

### CROSS REFERENCE TO RELATED APPLICATION

5        This application is based upon U.S. Provisional Patent  
Application, Serial No. 60/404,997, entitled "Variable Wattage  
Heater Control System", filed August 21, 2002, the contents of  
which are incorporated herein by reference in their entirety and  
continued preservation of which is requested.

### BACKGROUND OF THE INVENTION

#### 1.    Field of the Invention

10        The present invention relates to a control system, and  
particularly to a variable wattage control system. More  
15        specifically, the present invention relates to a variable wattage  
control system for a power-receiving device, such as the heating  
element.

#### 2.    Prior Art

20        Control systems for controlling the power output applied to a  
heating element or other power-receiving device are well known in  
the art. In particular, U.S. Patent Nos. 3,752,956 to Cahill et  
al.; 4,582,982 to Peigari; 4,894,520 to Moran; and 5,624,591 to Di  
Trapani all disclose some type of controller for controlling the  
25        power output to a heating element. Specifically, the Peigari  
reference teaches an SCR power controller in which the output

voltage to a resistance heater is varied in accordance with outside temperature, while the Moran reference applies a variable current to a resistance heater corresponding to variations in supply voltage by using a pulse width modulator which controls the timing of a switching device in order to control the flow of current through the resistance heater. Additionally, the Cahill et al. reference discloses a fixing circuit in arrangement with a gated triac and feeding circuits for controlling power output to a heating element. Finally, the Di Trapani reference teaches a control circuit comprising a triac for modulating the current supply to a heating element such that the flow of current is interrupted thereto when a predetermined threshold is reached.

However, further enhancements in power control systems are desirable. More specifically, there is a need in the art for a power controller that can convert at least one power-receiving device, such as a heating element, having a single wattage rating to a heating element having multiple wattage applications. There is a further need in the art for a controller that has the ability to limit the maximum wattage to a value less than that which would be provided at full line voltage, and which provides a scaling function for re-scaling the power output to the heating element in order to better control the power output. Further, there appears a need for a controller that permits manual input of various parameters for determining the desired scaling function by the

user. Further, there appears a need for a method of enhancing phase angle power control at low conduction angles.

#### OBJECTS AND SUMMARY OF THE INVENTION

5       The primary object of the present invention is to provide a variable wattage control system for controlling the power output to a power-receiving device by determining a scaling function that re-scales the power output such that the maximum wattage delivered to the power-receiving device can be less than that which would be  
10 provided at full line voltage. It will be understood accordingly that the new variable wattage control system is capable of scaling power to the power-receiving device even though the power ratings thereof may be less, or even considerably less than the power delivery capability of the new variable wattage control system.

15       Yet another object of the present invention is to provide a variable wattage control system that uses a single heater resistance value at many different wattage levels.

      Yet another further object of the present invention is to provide a variable wattage control system that allows the use of a  
20 power-receiving device at a lower than normal resistance by limiting the maximum voltage and current to a value less than that which would be supplied at full line voltage. The use of lower than normal resistance values can allow a power-receiving device to be designed with a resistive element of greater than normal

cross section, which can result in an increase in the life of the device.

Another further object of the present invention is to provide a variable wattage control system in which the power output of  
5 either the temperature or power controller is capable of being re-scaled.

A further object of the present invention is to provide a module for a variable wattage control system which is operatively associated with the power and temperature controllers of the  
10 control system for re-scaling the power output to the power-receiving device.

Another object of the present invention is to provide a novel enhancement of phase angle power control by allowing "off" cycles to occur between phase-angle-fired "on" cycles, thereby allowing  
15 an increase in the conduction angle of the phase-angle-fired "on" cycles.

The terms "heater" or "heating element" or "heat-producing element" or "heat producing means" as used herein are intended to mean generically any type of power-receiving device, whether as a  
20 single or plural unit, which is electrically powered, and may often be found in industrial heater context as an ohmic device comprising an electrically resistive element driven electrically to produce heat. However, the present invention contemplates that a power-receiving device may encompass any type of electrically

powered device including, but not limited to, a heating element or the like.

The terms "power control" or "power controller" or "power control means" as used herein are intended to mean generically any  
5 type of power control device normally found in heater control systems. Such devices include, but are not limited to, mechanical power switching devices (e.g., contactors, mercury displacement relays, etc.) and semiconductor power control (e.g., phase angle control, burst firing, pulse mode, pulse width modulation (PWM),  
10 etc., including conversion from AC power to DC and use of PWM from DC supply).

Another object of the present invention is to provide a variable wattage control system having a software-controlled subsystem that permits automatic or manual user input of various  
15 parameters into the variable wattage control system in order to determine a scaling function.

The terms "software" or "software subsystem" or "computer implemented software subsystem" or "software-controlled" as used herein are intended to include, but not limited to, imbedded  
20 software, which is also known as "firmware".

In brief summary, the present invention overcomes and substantially alleviates the deficiencies present in the art by providing a variable wattage control system comprising a power-receiving device connected to a power controller which is linked

to either a DC or AC power source for supplying power to the device. A sensing means is operatively associated with the power-receiving device for taking temperature readings and communicating those readings to a temperature controller. In the preferred embodiment, after the temperature readings are communicated to the temperature controller by the sensing means, the temperature controller then provides a re-scaled output to the power controller which limits and re-scales the amount of voltage applied to the power-receiving device. This method of limiting applied line voltage to the device and re-scaling the output sent to the device by the power controller permits multiple wattage values to be obtained from a single resistance value of the device. In other words, use by the variable wattage control system of a scaling factor based on the percentage of a full line voltage determines the maximum percentage power to be applied to the power-receiving device such that the device is not driven at a power level greater than its power level rating. The variable wattage control system of the present invention can be used accordingly to provide control of a wide variety of power-receiving devices such as heating elements, where the power rating of such elements or devices may be as great as that of the variable wattage control system or in fact may be substantially less, for the operation of the

variable wattage control system is protectively scaled for output according to the specifications of the element or device.

In accordance with one aspect of the present invention, a computer-implemented software subsystem is provided that permits  
5 the user to manually enter line voltage, element resistance (e.g., the ohmic value of a heater) and desired maximum power, in order to calculate a desired scaling factor. This scaling factor is applied by the software subsystem to re-scale the voltage output to the power-receiving device from the power controller. In this  
10 way, the user may change the scaling factor applied to the voltage output of the same power-receiving device in order to obtain multiple maximum wattage values therefrom, or else to power many possible elements or devices, each having a different rating.

The terms "computer" or "computer implemented" or "micro-  
15 controller" as used herein are intended to include microprocessors, micro-controllers, digital signal processors, programmable logic arrays, and any other device capable of performing programmed instructions.

Preferably, the software subsystem for determining the  
20 scaling factor is found in the temperature controller; however, the present invention contemplates that the software subsystem can be contained within the power controller or other suitable device. The scaling factor function may alternatively be contained in a special module arrangement which is operatively associated between

the power controller and the power-receiving device, or between the voltage source and the power controller, or between the temperature controller and the power controller for accomplishing the same function. The scaling factor of such a special module may  
5 be pre-set at the place of manufacture or may be field adjustable.

As noted above, the variable wattage control system of the present invention uses a single heater resistance value with the power-receiving device to achieve many different wattage values by controlling the voltage and current applied to the device.

10 Further, the present invention controls the line voltage and current applied to the power-receiving device to values less than would otherwise be supplied at full line voltage and re-scales this output to the device. For example, a user that requires the same physical size heating element in four different

15 voltage/wattage combinations: 500 watt and 600 watt at both 120V and 240V would have to purchase the following four different heating elements having the same physical size: (A) 500 watts, 120V, 28.8 ohms; (B) 500 watts, 240V, 115.2 ohms; (C) 600 watts, 120V, 24.0 ohms; and (D) 600 watts, 240V, 96.0 ohms. By using the

20 variable wattage control system of the present invention, these four types of heating element parameters A, B, C, and D can be effectively replaced with heating elements of a single resistance value by limiting the heating element voltage to a value less than full line voltage and re-scaling the heating element voltage to

supply the desired wattage. The variable wattage control system of the present invention may work with any kind of known techniques of AC or DC semiconductor power control (e.g., phase angle control, burst firing, pulse mode, pulse width modulation

5 (PWM), power transistors, etc., including conversion from AC power to DC and use of PWM from DC supply) or mechanical power switching devices (e.g., contactors, mercury displacement relays, etc.).

When used with a phase angle power control system, the present invention may include a method of improving phase angle power  
10 control in order to enhance the accuracy of phase angle power control at low conduction angles. The present invention may use phase angle power control, but not does not necessarily require the use of such a power control system.

Additional objects, advantages and novel features of the  
15 invention will be set forth in the description which follows, and will become apparent to those skilled in the art upon examination of the following more detailed description and drawings in which like elements of the invention are similarly numbered throughout.

#### 20 BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a simplified block diagram of the preferred embodiment of the variable wattage control system showing the control system implemented in a temperature controller according to the present invention;

FIG. 2 is a flow chart illustrating the method for determining the scaling factor and re-scaling the power output to the power-receiving device by the temperature controller according to the present invention;

5        FIG. 3 is a simplified block diagram of an alternative embodiment of the variable wattage control system showing the control system implemented in a power controller according to the present invention;

FIG. 4 is a flow chart illustrating the method for  
10 determining the scaling factor and re-scaling the power output to the power-receiving device by the power controller according to the present invention;

FIG. 5 is a simplified block diagram of an alternative embodiment of the variable wattage control system showing the  
15 control system implemented in a combined temperature/power controller according to the present invention;

FIG. 6 is a flow chart illustrating the method for manually or automatically determining the scaling factor and re-scaling the power output to the power-receiving device by the combined  
20 power/temperature controller according to the present invention;

FIG. 7 is a simplified block diagram of an alternative embodiment of the variable wattage control system showing the control system implemented in a module according to the present invention;

FIG. 8 is a simplified block diagram showing the control system implemented in the module having an alternative circuitry arrangement according to the present invention;

FIG. 9 is a simplified block diagram showing the control system implemented in the module having an alternative circuitry arrangement according to the present invention and

FIG. 10A-C are graphs illustrating the enhancement to a phase angle fire control system according to the present invention.

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#### DETAILED DESCRIPTION OF THE INVENTION

Referring to the drawings, the preferred embodiment of the variable wattage control system is illustrated and generally indicated as 10 in FIG. 1. Variable wattage control system 10 comprises a power controller 12 linked to a AC or DC voltage source 20 for providing a power output to a power-receiving device, such as a heat-producing means 16. A sensing means 18 senses the environmental temperature associated with the heat-producing means 16 and communicates temperature readings to a temperature controller 14 which is operatively associated with the power controller 12.

According to one aspect of the present invention, variable wattage control system 10 provides a means for controlling the power output from the power controller 12 to the heat-producing

means 16 by limiting and re-scaling the amount of line voltage applied to the heat producing means 16. Preferably, temperature controller 14 includes a micro-controller 23 which embodies a software subsystem 30 (FIG. 2) for calculating and communicating a signal to the power controller 12 that controls the power output to the heat-producing means 16 as shall be discussed in greater detail below. In the alternative, if the system does not include a software subsystem 30 to implement the scaling function, the scaling function may be preset by the manufacturer or may be field adjustable, such as through the use of one or more switches.

Referring to FIG. 2, software subsystem 30 provides a routine that instructs the temperature controller 14 to obtain new input from the user through a user interface (not shown) in order to generate a power output scaling factor,  $K_{out}$ , and produce a signal 84 to power controller 12. The term "user interface" as used herein is intended to include manual inputs (e.g., keypads), and electronic means (e.g., wired or wireless communication buses and electronic storage media) or any suitable means to transfer the pertinent information to the software subsystem 30. At steps 32, 34 and 36, respectively, the user enters the line voltage (in  $V_{rms}$ ) produced by voltage source 20, the resistance value (in Ohms) of heating-producing means 16, and the desired power (in Watts) to be applied to heating-producing means 16. Once the line voltage, resistance value and desired power values are entered

into the temperature controller 14, the micro-controller 23, at step 38, calculates the power at full line voltage using the following equation:

5 
$$P_{line} = \frac{(V_{line})^2}{R_{heater}}$$

After  $P_{line}$  is determined, the micro-controller 23, at step 40, calculates the power output scaling factor,  $K_{out}$ , using the  
10 following equation:

$$K_{out} = \frac{P_{desired}}{P_{line}}$$

15 In the alternative, the power output scaling factor,  $K_{out}$ , may be entered through the user interface instead of calculated in the software sub-system 30. Once the power output scaling factor has been determined, the sensor 18 takes a temperature reading and communicates that reading to the micro-controller 23 at step 42.  
20 The micro-controller 23, at step 44, compares the temperature reading to a temperature set point previously established by the user. The required percentage power output level,  $P_{out}$ , is determined by the temperature controller 14 in the normal manner at step 44, and then the micro-controller 23 calculates a scaled

percentage power output,  $P_{out\ scaled}$ , at step 46, using the following equation:

$$P_{out\ scaled} = P_{out} * K_{out}$$

5       After the scaled power output,  $P_{out\ scaled}$ , has been calculated, the micro-controller 23 instructs the temperature controller 14 to communicate a signal 84 to the power controller 12 establishing the desired power output to the heat producing means 16. Power controller 12 receives signal 84 and provides the proper power  
10   output to the heat-producing means 16. Signal 84 is a control signal having a signal level appropriate for communicating the desired power output to the power controller 12. The level of signal 84 signifies the level of power output to be provided by power controller 12 to heat-producing means 16. For example, a  
15   resistive heating element of 24 Ohms is desired to be operated as a 1200 Watt heating element at a line voltage of 240 Vrms. This 24 Ohm heating element supplies 2400 Watts at full line voltage. A temperature controller 14 with a linear 4-20 mA output range, without applying the scaling factor,  $K_{out}$ , of the present invention  
20   for re-scaling the power output at full line voltage, the strength of signal 84 for a 4mA signal = 0 power level; 12mA signal = 50% power level or 1200 Watts; and 20ma signal = 100% power level or 2400 Watts representing full line voltage being applied to the heat producing means 16. When the scaling factor,  $K_{out}$  is

calculated to be 0.5 and is applied to this scheme 4mA still represents 0 power level; however, 8mA = 50% power level or 600 Watts and 12mA = 100% power level or 1200 Watts. Therefore, a 12mA signal 84 to the power controller 12 will provide a scaled power  
5 output of 100% of the desired wattage (1200 Watts) or 50% of the full line power of 2400 Watts. However, the present invention contemplates that other scaling factors will produce different schemes, for example, a 0.25 or 25% scaling factor will produce a 8mA signal 84 to the power controller 12 representing a scaled  
10 power output of 100% or 25% of the full line voltage power.

After  $P_{out \text{ scaled}}$  is determined, the power controller 12 sets the scaled power output to the heat-producing means 16 to a level that equals  $P_{out \text{ scaled}}$  in step 48. However, if no new scaling factor is being implemented, the software subsystem 30 returns to step 42  
15 for another temperature reading and power output calculation. The loop from step 48 back to step 42 is repeated until the user interrupts the loop, such as to enter new data in steps 32 through 36.

Referring to FIG. 3, an alternative embodiment 110 of the  
20 variable wattage control system is illustrated. In this particular embodiment, variable wattage control system 110 comprises substantially the same arrangement as the preferred embodiment, except software subsystem 130 is found in a micro-controller 123 which is operatively associated with the power controller 12,

rather than the temperature controller 14. In the alternative, if the variable wattage control system 110 does not include a software subsystem 130 to implement the scaling function, the scaling function may be preset by the manufacturer or may be field  
5 adjustable, such as through the use of one or more switches.

As shown in FIG. 4, software subsystem 130 provides a routine that instructs the power controller 12 to obtain new input from the user through a user interface (not shown) at controller 12 in order to generate a power output scaling factor,  $K_{out}$ , and produce  
10 a scaled power output to the heat-producing means 16. At steps 50, 52, and 54, respectively, the user enters the line voltage (in  $V_{rms}$ ) produced by voltage source 20, the resistance value (in Ohms) of heat-producing means 16, and the desired power (in Watts) to be applied to heat-producing means 16. In the alternative,  
15 power controller 12 may automatically read the existing line voltage from voltage source 20 as well as the resistance value of heat-producing means 16 without user input. Once the line voltage, resistance value and desired power values are entered into the power controller 12, the micro-controller 123, at step  
20 56, calculates the power at full line voltage using the same equation for determining  $P_{line}$  as was calculated in the preferred embodiment. After  $P_{line}$  is determined, the micro-controller 123, at step 58, calculates the power output scaling factor,  $K_{out}$ , also using the same equation utilized in the preferred embodiment. In

the alternative, the power output scaling factor,  $K_{out}$ , may be entered through the user interface instead of calculated in the software sub-system 130. Once the power output scaling factor has been determined, the power controller 12 reads a signal 84  
5 communicated by the temperature controller 14. Signal 84 is a control signal having a level which represents the percentage power output required to reach a certain set point temperature established in the temperature controller 14. This is based on the temperature reading communicated by the sensing means 18,  
10 comparing that reading against a set point temperature and providing the above signal 84 to the power controller 12. After the micro-controller 123 reads the signal 86 sent by the temperature controller 14 a new percentage power output,  $P_{out\ scaled}$ , is calculated at step 62, using the same equation noted in step  
15 46. After  $P_{out\ scaled}$  is determined, the power controller 12 sets the power output to the heat-producing means 16 to a level that equals  $P_{out\ scaled}$ . However, if no new power output scaling factor is being implemented, the software subsystem 130 returns to step 60 for another temperature controller 14 reading and power output  
20 calculation. The loop from step 64 back to step 60 is repeated until the user interrupts the loop, such as to enter new data in steps 50 through 54.

Referring to FIG. 5, an alternative embodiment 210 of the variable wattage control system is shown. In this arrangement, the

power controller 12 and temperature controller 14 are combined into a single combined controller 22 which receives temperature readings from the sensor 18 and provides a limited and scaled power output to the heat-producing means 16. In the alternative, if the system 210 does not include a software subsystem to implement the scaling function, the scaling function may be preset by the manufacturer or may be field adjustable, such as through the use of one or more switches. As shown in FIG. 6, software subsystem 230 provides a routine that instructs the combined controller 22 to obtain new input from the user through a user interface (not shown) at controller 22 in order to generate a power output scaling factor,  $K_{out}$ , and produce a scaled power output to the heat-producing means 16. At steps 66, 68, and 70, respectively, the user enters the line voltage (in Vrms) produced by voltage source 20, the resistance value (in Ohms) of heat-producing means 16, and the desired power (in Watts) to be applied to heat-producing means 16. In the alternative, combined controller 22 may automatically read the existing line voltage from voltage source 20 as well as the resistance value of heat-producing means 16 without user input.

Once the line voltage, resistance value and desired power values are entered or read into the combined controller 22, the micro-controller 223, at step 72, calculates the power at full line voltage using the same equation for determining  $P_{line}$  as was

discussed above. After  $P_{line}$  is determined, the micro-controller 223, at step 74, calculates the power output scaling factor,  $K_{out}$ , also using the same equation discussed above. Once the power output scaling factor has been determined, the combined controller 22, at step 76, reads the temperature being communicated by sensor 18. At step 78, the micro-controller 223 compares the temperature reading against a predetermined set point temperature and calculates the required percentage power output level,  $P_{out}$ , in the normal manner, and then the micro-controller 223 calculates a scaled percentage power output  $P_{out\ scaled}$  at step 80, using the same equation noted in the other embodiments. After the scaled power output  $P_{out\ scaled}$  is determined, the combined controller 22 sets the power output to the heat-producing means 16 to a level that equals the new scaled power output,  $P_{out\ scaled}$ . However, as in the other embodiments, if no new power output scaling factor is being implemented, the software subsystem 230 returns to step 76 for another temperature reading and power output calculation. The loop from step 82 back to step 76 is repeated until the user interrupts the loop, such as to enter new data in steps 66 through 70.

Referring to FIG. 7, an alternative embodiment 310 of the variable wattage control system is illustrated. In this particular embodiment, variable wattage control system 310 comprises a module 24 having one connection to power control means 12 and a second connection to heat-producing means 16, while temperature

controller 14 provides an output signal 84 to power control means 12. Power control means 12 then supplies a voltage and current to Module 24. As further shown, module 24 then supplies a scaled voltage and current to heat-producing means 16 that is less than  
5 the voltage and current that would otherwise be supplied by power control means 12 alone. Although module 24 could be implemented through a micro-controller subsystem, module 24 does not require a micro-controller or software subsystem to calculate and set the scaled power output to the heat producing means 16. The power  
10 output scaling factor  $K_{out}$  can be preset by the manufacturer or set by manual means on module 24, such as by one or more switches. The power output to the heat-producing means 16 is limited through a solid state device (e.g. triac, SCR, solid state relay, power transistor, etc.) inside the module 24 that is set at a  
15 predetermined level in order to limit the power output to heat-producing means 16.

Referring to FIG. 8, an alternative embodiment 410 of the variable wattage control system is illustrated. In this particular embodiment, variable wattage control system 410 comprises a module  
20 24 having one connection to voltage source 20 and a second connection to power control means 12. Voltage source 20 supplies a voltage and current to module 24 which then supplies a scaled voltage and current to power control means 12. As further shown, temperature controller 14 provides an output signal 84 to power

control means 12. Power control means 12 then supplies a scaled voltage and current to heat-producing means 16 that is less than the voltage and current that would otherwise be supplied without module 24. Although module 24 could be implemented through a micro-controller subsystem, module 24 does not necessarily require a micro-controller or software subsystem to calculate and set the scaled power output to the heat-producing means 16. The power output scaling factor  $K_{out}$  can be preset by the manufacturer or set by manual means on module 24, such as by one or more switches. The power output to the heat-producing means 16 is limited through a solid state device (e.g. triac, SCR, solid state relay, power transistor, etc.) inside the module 24 that is set at a predetermined level in order to limit the power output to heat-producing means 16.

Referring to FIG. 9, another alternative embodiment 510 of the variable wattage control system is shown. In this particular embodiment, variable wattage control system 510 substantially comprises the same configuration as the variable wattage control system 10 shown in FIG. 1; however, a module 124 is operatively interposed between the output to the temperature controller 14 and the input to the power control means 12. In this configuration, module 124 receives signal 84 from the temperature controller 14 and provides a predetermined limited and scaled output to the power control means 12. Although module 124 could be implemented

through a micro-controller subsystem, module 124 does not necessarily require a micro-controller or software subsystem to calculate and set the power output scaling factor  $K_{out}$  to the power control means 12. The power output scaling factor can be preset by  
5 the manufacturer or set by manual means on module 124, such as by one or more switches.

When applied to a phase angle power control system, the present invention results in lower than normal conduction angles due to the power limiting function. Because of the nature of phase  
10 angle fired devices, such as SCR's, power control at low conduction angles can be less accurate than power control at higher conduction angles. In order to ameliorate the problems associated with low conduction angles, the present invention offers an enhancement to phase angle power control at low  
15 conduction angles, or when phase angle control is combined with burst firing. This allows "off" cycles to occur between phase-angle-fired "on" cycles, thereby allowing an increase in the conduction angle of the phase-angle-fired "on" cycles. Referring to FIG. 10A, a normal phase angle power controller receiving a  
20 command for 7% power would have a conduction phase angle of 41 degrees on every ac line cycle. Using the present invention and phase angle firing every other ac line cycle, a 7% power output is attained with a 53 degree conduction angle as illustrated in FIG. 10B. Further, as shown in FIG 10C, phase angle firing every third

ac line cycle using the present invention, a 7% power output is attained with a 62 degree conduction angle. Preferably, this aspect of the present invention is an enhancement to the power control means 12 in FIGS. 1 and 3, or, in the alternative, to  
5 combined temperature/power controller 22 shown in FIG. 5 or module 24 shown in FIGS. 7 and 8.

Thus, it is seen that the present invention provides a variable wattage control system 10 for providing varying wattage levels for at least one power receiving device such, as a heat-  
10 producing means 16. The control system 10 preferably comprises at least one heat-producing means 16 operatively associated with a temperature sensing means 18; the temperature sensing means 18 communicating with a temperature controller 14 for comparing the sensed temperature with a desired set point; a power control  
15 means 12 of the temperature controller 14, for providing energization of the heating element 16 at a selected maximum wattage level; and the temperature controller 14 being operative such that, if the sensed temperature, when compared to the set point, indicates that the control system 10 requires heat, the  
20 temperature controller 14 directs a power control means 12 to turn on the heat-producing means 16 at a specific maximum wattage level. The variable wattage control system 10 may further comprise a micro-controller 23 which determines a power output scaling factor based on the percentage of a full line

voltage being applied to the heating element 16 and then scales the power output accordingly; the power output scaling factor determining the maximum percentage power to be applied to the heating element 16. Accordingly, at least one heat-producing means 16 (whether a single or plural unit) may be driven at different power levels for various applications, and where the power rating of the variable wattage control system 10 can be greater than the power rating of the heat-producing means 16.

It is also thus seen that there is described herein a method of using a variable wattage heater control system 10 for providing varying wattage levels for a heat-producing means 16, where the heat-producing means 16 may be required to be driven at power levels less than the power level capability of the variable wattage control system 10, comprising using a temperature sensing means 18 for measurements of a temperature associated with the heat-producing means 16 during operation thereof; providing the temperature measurements to a temperature controller 14 for comparing the temperature measurements with a desired set point; using a power control means 12 of the temperature controller 14, for providing energization of the heat-producing means 16 at a selected maximum wattage level; the temperature controller 14 operating such that, if the sensed temperature, when compared to the set point, indicates that the system 10 requires heat, the temperature controller 14 directs a

power controller 12 to turn on the heat-producing means 16 at a specific maximum wattage level; and using a micro-controller 23 to determine a power output scaling factor based on the percentage of a full line voltage being applied to the heat-producing means 16 and then scaling the power output accordingly as well as causing the power output scaling factor to determine the maximum percentage power to be applied to the heat-producing means 16 such that the heat-producing means 16 is not driven at a power level greater than its power level rating.

According to a further aspect of the present invention in the foregoing method for determination of the scaling factor, the method further comprises providing the scaling factor to the micro-controller through a user interface or electronic communication techniques.

According to a further aspect of the present invention in the foregoing method for determination of the scaling factor, the method further comprises providing to the micro-computer the line voltage of a power source for the power controller, electrical resistance of the heat-producing means 16 and desired maximum power of the heat-producing means 16.

Such values can be determined and manually entered or might be automatically determined, or provided through electronic communications techniques, or provided by information stored in a look-up table or otherwise reported by characteristics or

features of the heat-producing means 16, such as by test or surrogate test device energization, or by fixture specification or determination, to the variable wattage control system 10.

Various precautions and operating limitations and safety  
5 features will be appropriate for skilled users making industrial application of the new system. For example, and without limitation, the variable wattage control system 10 typically can be provided with short-circuit or "full on" over-current protection or so-called "crowbar" circuit protection where the  
10 system is to make use of semiconductor-controlled devices, such as SCR's (thyristors) or bidirectional switching devices (triacs), which could fail in a shorted condition.

Further, in the case of the variable wattage control system  
10 of the invention which uses phase angle controlled AC or pulsating DC control, special filtering may be used to suppress  
15 high frequency component generation in order to comply with product certification protocols or regional or approval agency criteria, such as health, safety and environmental rules or specifications establishing criteria which such devices or  
20 systems must meet to qualify for CE (Conformite Europeene) marking regulations for devices used and marketed in the European Union.

Variable wattage control system 10 of the present invention may, of course, use any of the previous power-control methods or

switching protocols, such as PWM or phase control, according to whether the system 10 can be powered by a utility with regulations relating to types of power control schemes, or operating limitations thereon.

5           Further, in the use of the variable wattage control system 10 according to the present invention, appropriate care can be taken by those skilled in the use of the invention to avoid deleterious effects on power factor which may be of concern to utilities supplying power to be controlled by the system 10.

10           As a further example, rather than sensing temperature of a power-receiving device, power output or tractive force or angular velocity (as of a motor shaft) of another type of power-controlled device may be measured and applied to a device or circuit analogous to the temperature measuring and controlling  
15 means 18 or circuits of the invention, but wherein the power controller 12 provides a scaled output to the power-controlled device consistent with the principles of the invention.

          It should be understood accordingly from the foregoing that, while particular embodiments of the invention have been  
20 illustrated and described, various modifications can be made thereto without departing from the spirit and scope of the present invention. Therefore, it is not intended that the invention be limited by the specification; instead, the scope of

the present invention is intended to be limited only by the  
appended claims.